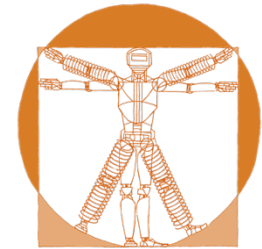


2011

summer school on impedance



extroduction



Deutsches Zentrum
für Luft- und Raumfahrt e.V.
in der Helmholtz-Gemeinschaft

leftovers from this week

1. do robots need biarticulate muscles?
2. what impedance do we need, really?
let us
 - measure human arm impedance
 - measure impedance during movement
 - estimate impedance from EMG
3. can we control position out of pns/cns signals?



my issue

learn, but
do not copy
or mimic!

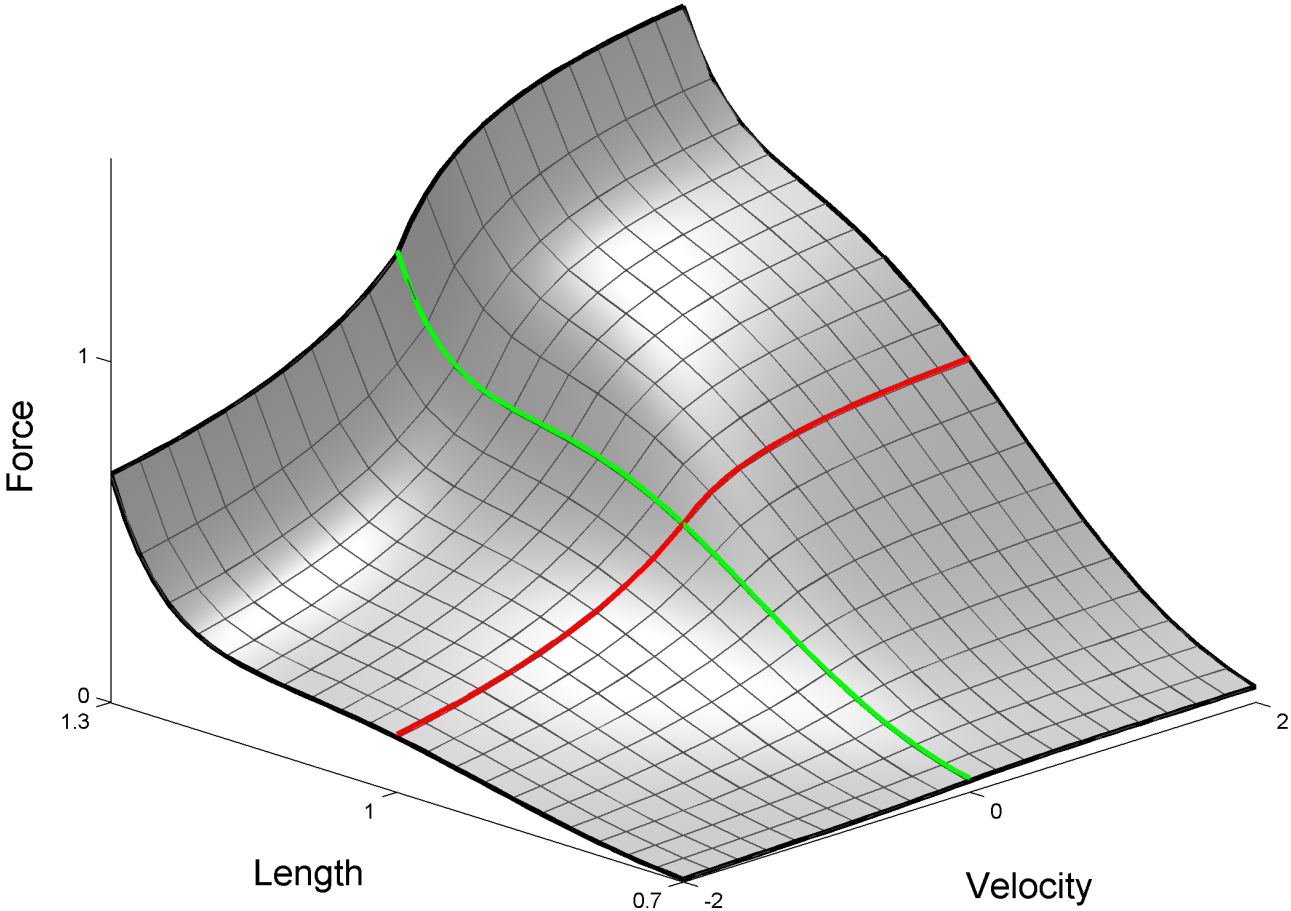


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do robots need biarticulate muscles?



muscle \neq torque motor



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dominic lakatos

□ Ph.D candidate

□ research topic: human
impedance & control
of variable-impedance
robots



arm model

- rigid body dynamics of the arm

$$\Gamma(\mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}, \boldsymbol{\xi}) = \mathbf{M}(\mathbf{q}, \boldsymbol{\xi}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \boldsymbol{\xi}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}, \boldsymbol{\xi})$$

- muscle impedance

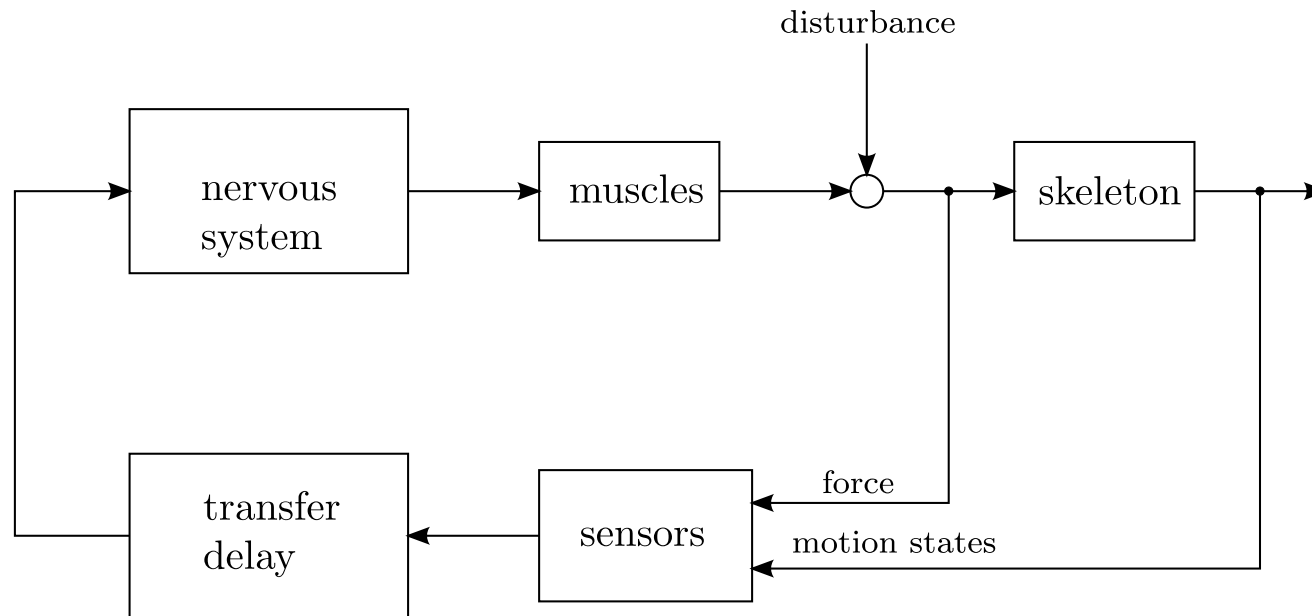
$$\boldsymbol{\tau}_{\text{muscles}} = \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{a})$$

- complete system torque

$$\mathbf{M}(\mathbf{q}, \boldsymbol{\xi}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \boldsymbol{\xi}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}, \boldsymbol{\xi}) + \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{a}) = \boldsymbol{\tau}_{\text{ext}}$$



we want to measure the arm, not the brain



- stretch reflex: 25-50ms
- spinal reflex: 70-110ms
- long-latency reflex: >110ms



locally linearised impedance

□ Taylor approximation to h can be written as

$$\mathbf{h}^* = \mathbf{h}|_{\mathbf{q}_0, \mathbf{a}_0} + \left. \frac{\partial \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{a})}{\partial \mathbf{q}} \right|_{\mathbf{q}_0, \mathbf{a}_0} \Delta \mathbf{q} + \left. \frac{\partial \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{a})}{\partial \dot{\mathbf{q}}} \right|_{\mathbf{q}_0, \mathbf{a}_0} \Delta \dot{\mathbf{q}} + \left. \frac{\partial \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{a})}{\partial \mathbf{a}} \right|_{\mathbf{q}_0, \mathbf{a}_0} \Delta \mathbf{a}$$

□ since the activation is assumed to be constant

$$\mathbf{h}^* = \mathbf{K} \Delta \mathbf{q} + \mathbf{D} \Delta \dot{\mathbf{q}}$$

□ in the transversal plane the gravity=0

$$\underbrace{\mathbf{M}(\mathbf{q}, \xi) \ddot{\mathbf{q}} + (\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \xi) + \mathbf{D}) \dot{\mathbf{q}} + \mathbf{K} \Delta \mathbf{q}}_{\Psi(\ddot{\mathbf{q}}, \dot{\mathbf{q}}, \Delta \mathbf{q}, \xi, \mathbf{D}, \mathbf{K},)} = \Delta \boldsymbol{\tau}_{\text{ext}}$$



linear parameter identification model

□ parameter vector

$$\zeta = [\xi_1, \xi_2, \xi_3, D_{11}, D_{12}, D_{21}, D_{22}, K_{11}, K_{12}, K_{21}, K_{22}]^T$$

□ identification model

$$\mathbf{W} \zeta = \mathbf{y}$$

$$\mathbf{W} = \begin{bmatrix} \mathbf{X}(1) \\ \mathbf{X}(2) \\ \vdots \\ \mathbf{X}(N) \end{bmatrix}, \quad \mathbf{y} = \begin{bmatrix} \Delta \tau_{\text{ext}}(1) \\ \Delta \tau_{\text{ext}}(2) \\ \vdots \\ \Delta \tau_{\text{ext}}(N) \end{bmatrix}$$

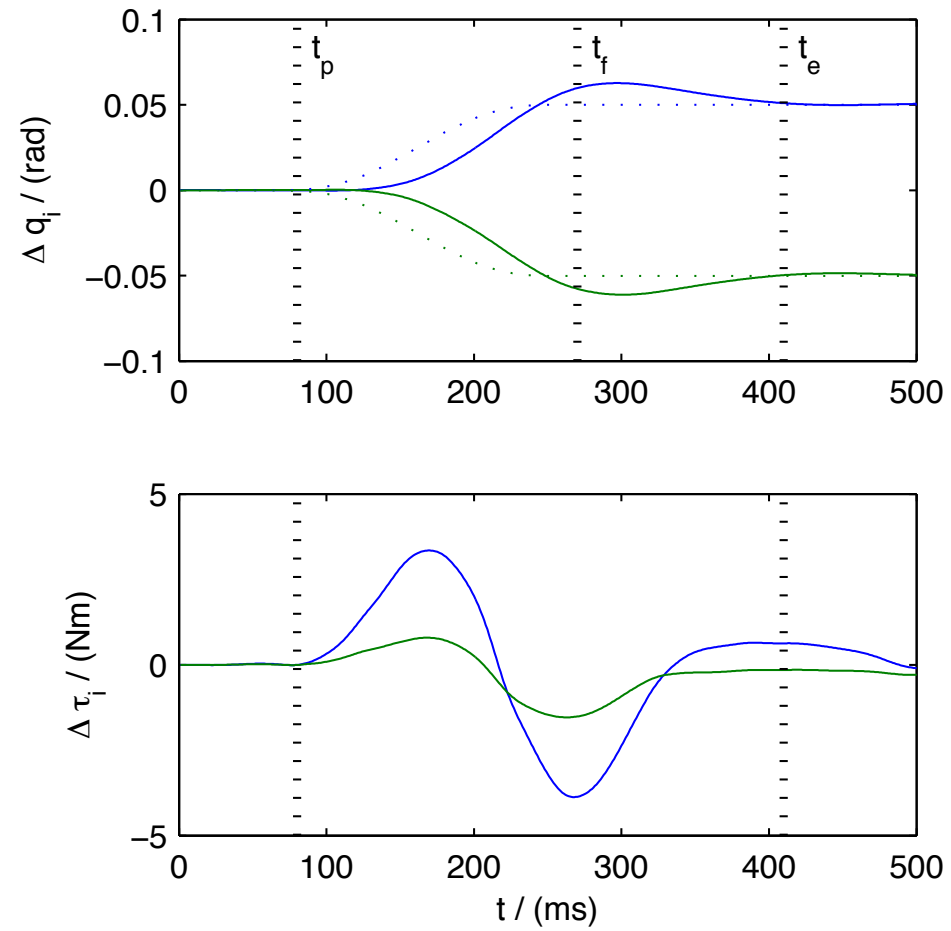
$$\mathbf{X} = \left(\frac{\partial \Psi(\ddot{\mathbf{q}}, \dot{\mathbf{q}}, \Delta \mathbf{q}, \boldsymbol{\xi}, \mathbf{D}, \mathbf{K},)}{\partial \zeta} \right)$$



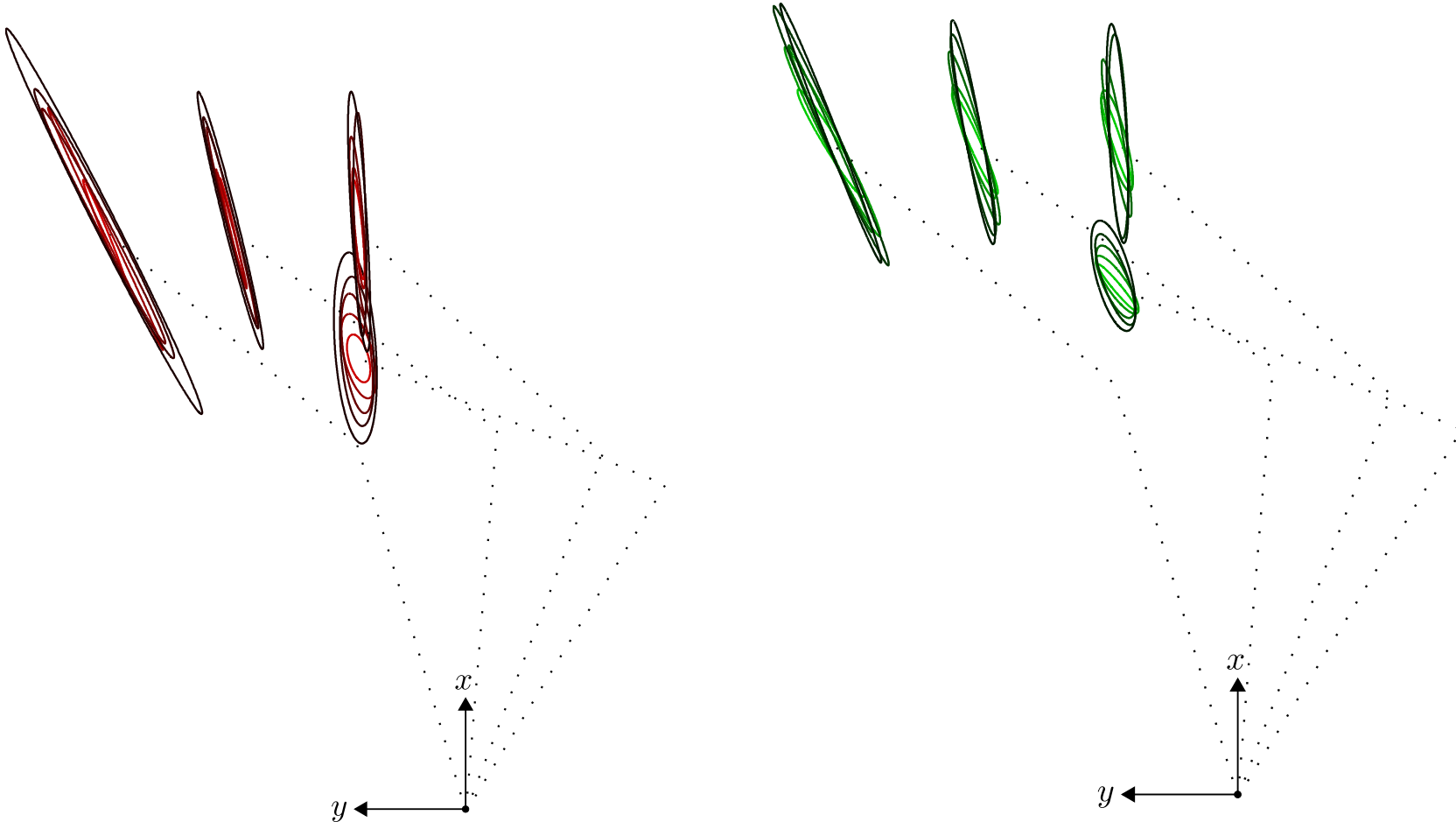
experimental setup



perturbations



resulting stiffness and damping



we're not there yet...

- what will these look like in 3D?
- how do we measure intrinsic tendulomuscular properties?
- how can we map these to EMG activities?



leftovers from this week

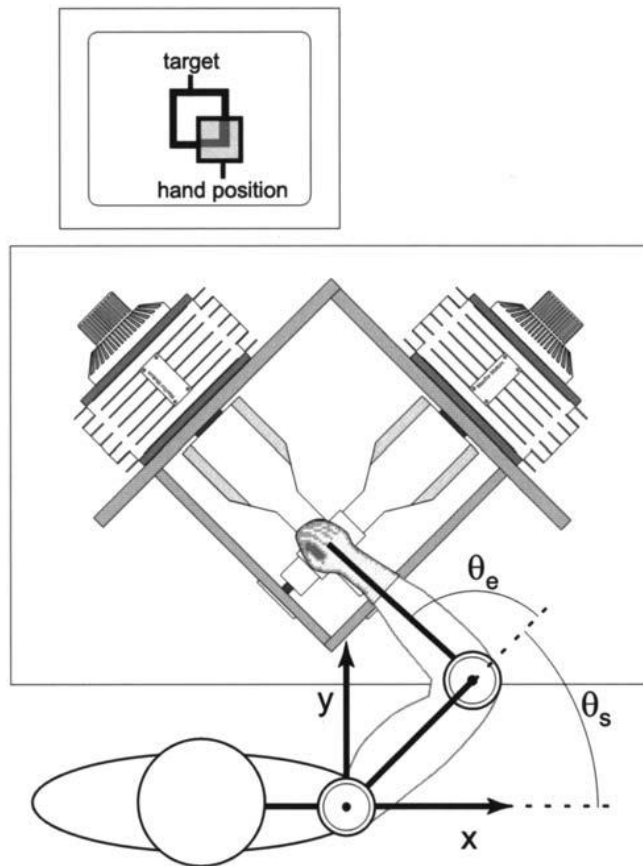
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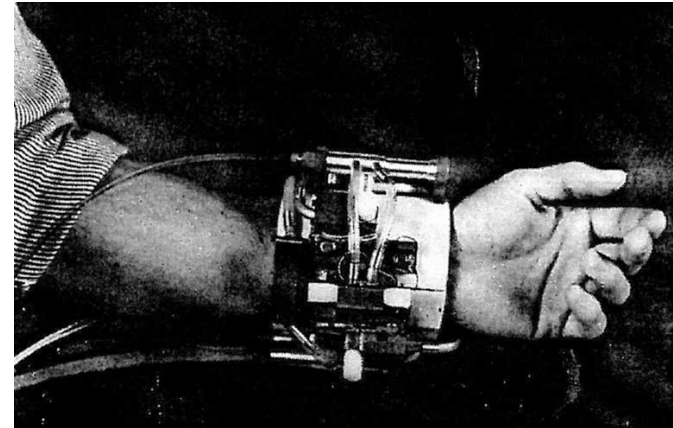
hannes höppner [hupna]



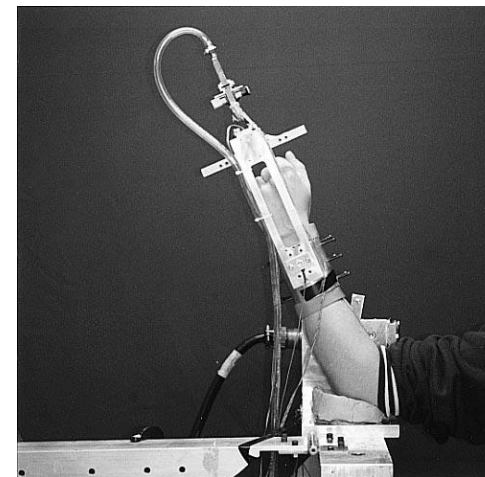
related work



Adaptive control stiffness to stabilize hand position with large loads [Franklin03]



The Design of a Dynamics Measuring Device [Colg86]



A Robust Ensemble Data Method for identification of Human Joint Mechanical Properties During Movement [Xu99]



related work

drawbacks of existing solutions measuring arm stiffness

position-perturbation setups

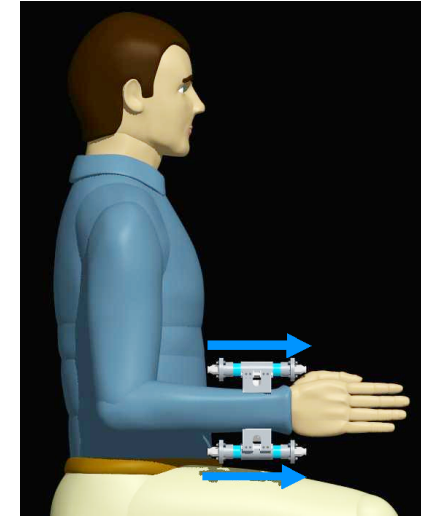
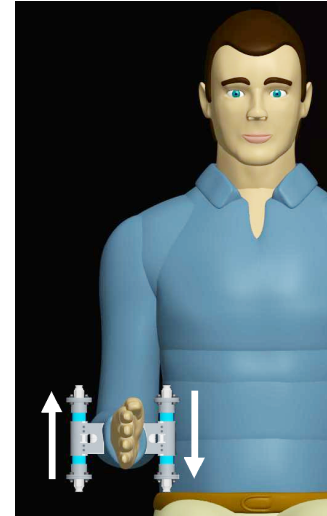
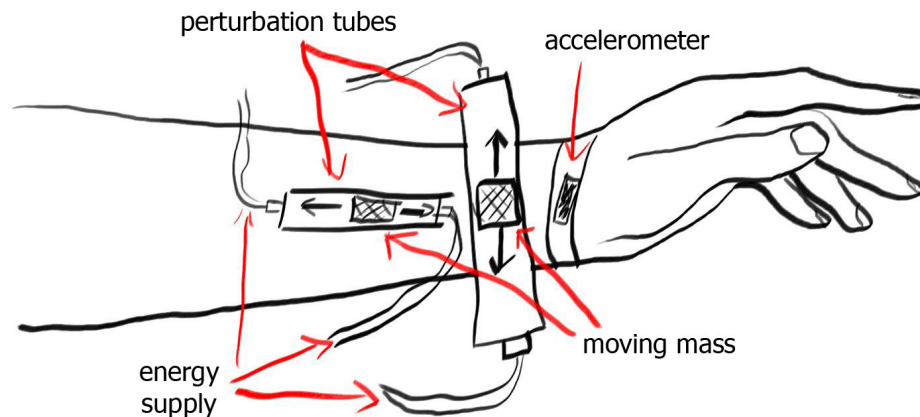
- not wearable
- unnatural constrained and only planar movements

wearable force-perturbation setups

- only force less than 6N
- Influence of heavy loads during common tasks can not be identified clearly
- Precise control of this devices seems to be problematic



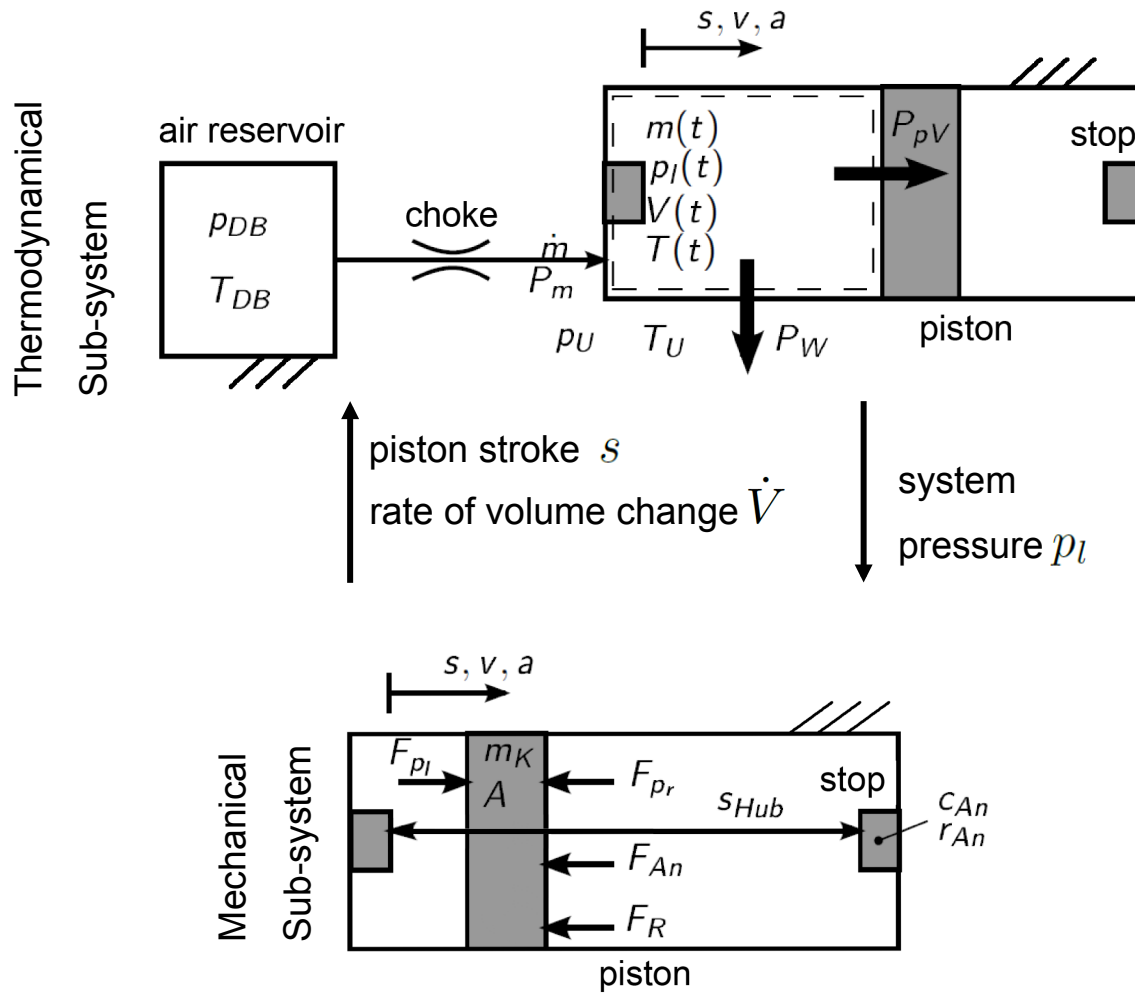
Idea and Specifications



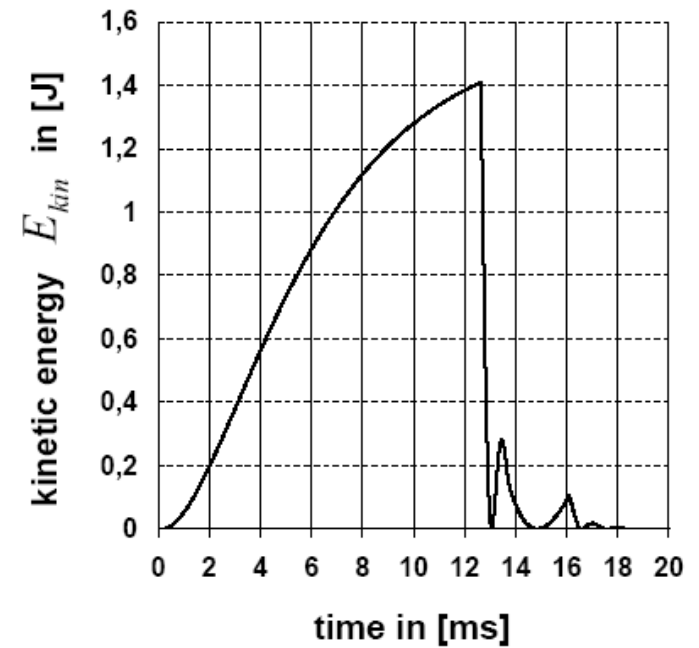
- accelerating and decelerating a mass inside a tube fixed to the limb
- energy is induced using external energy reservoir; here: compressed air
- using defined impact $<25\text{ms}$
- 2 perturbation tubes to induce clear rotations and translations



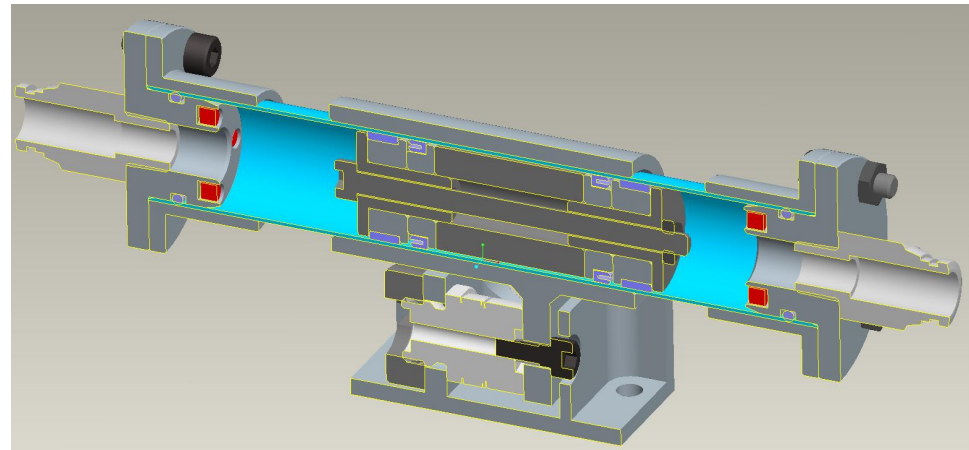
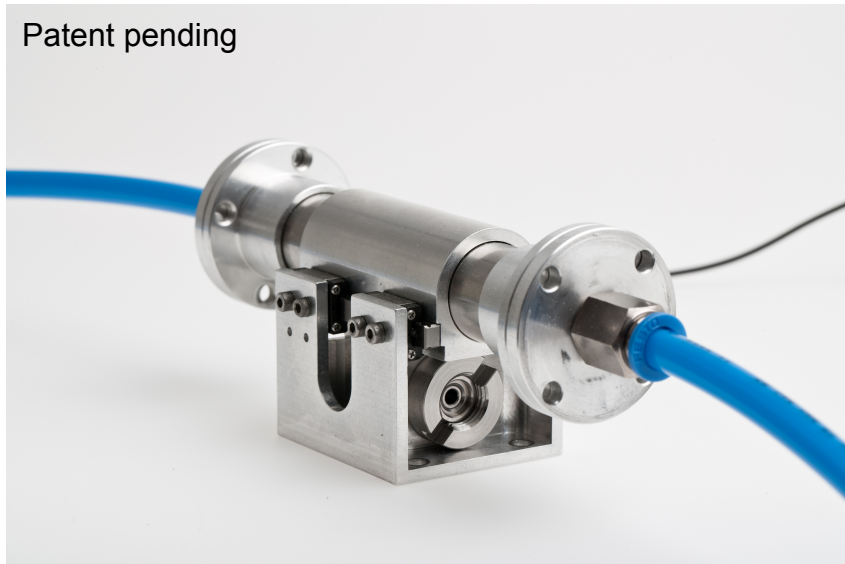
modeling and simulation



Goal: optimize measurement time and total mass



implementation

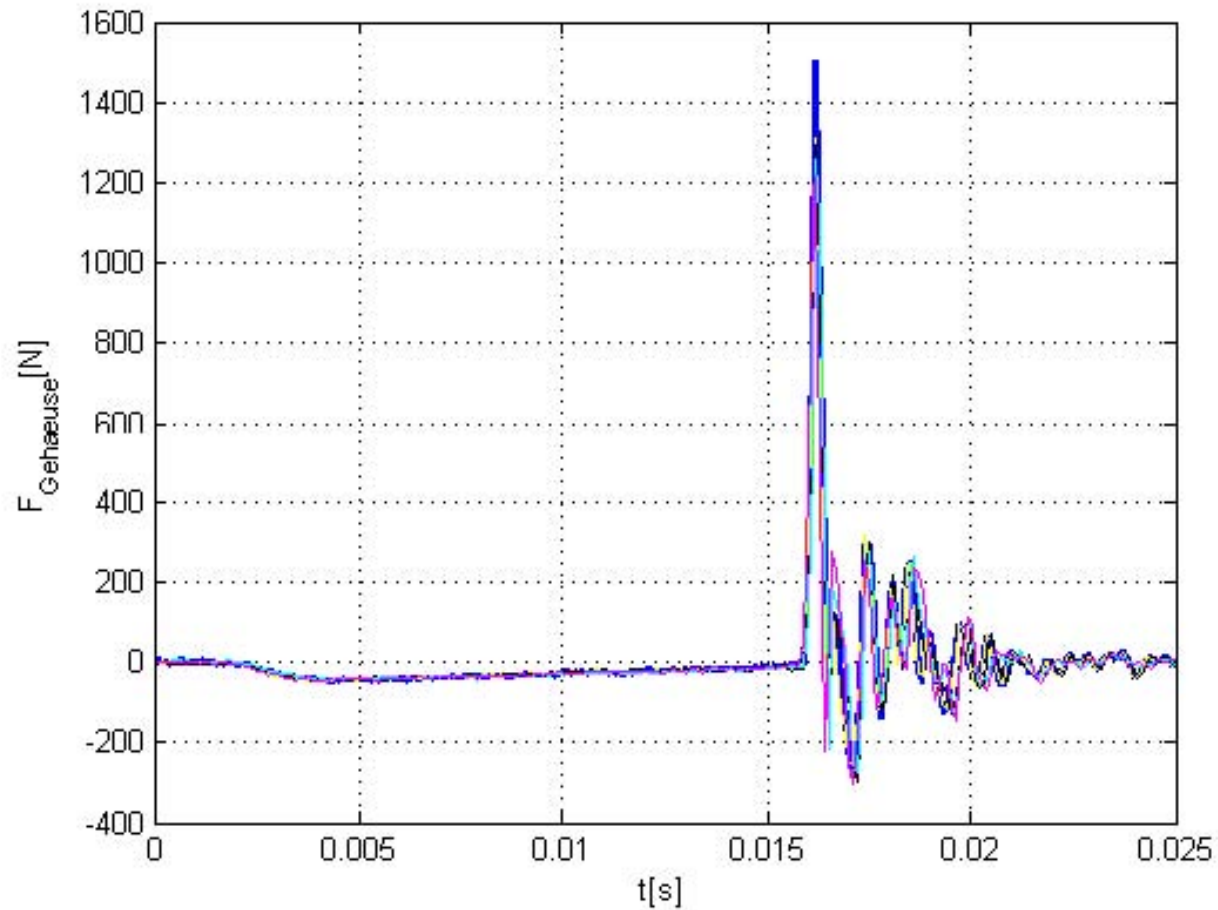


- steel tube length of 130mm and 300g weight
- two external relays
- mass consists of sealing, sliding and inertia elements
- magnets to increase the counterforce against the air pressure
- additional force sensor between arm and Perturbator tube



results on device properties

Measured and simulated force



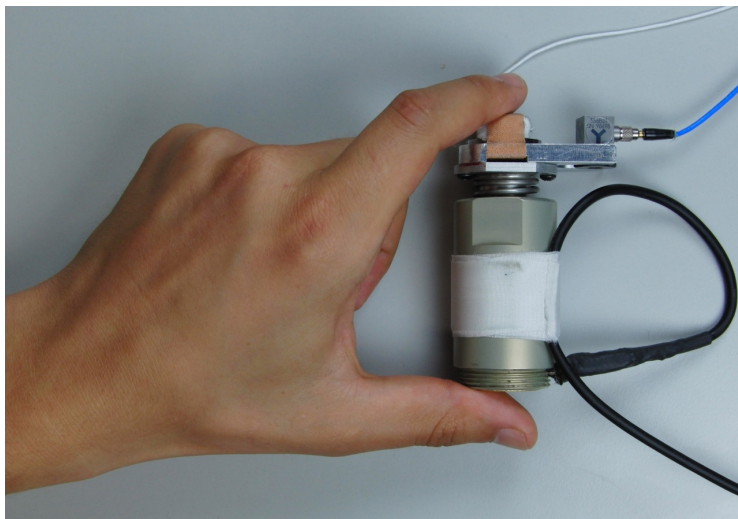
measuring human grasp stiffness

Requirements

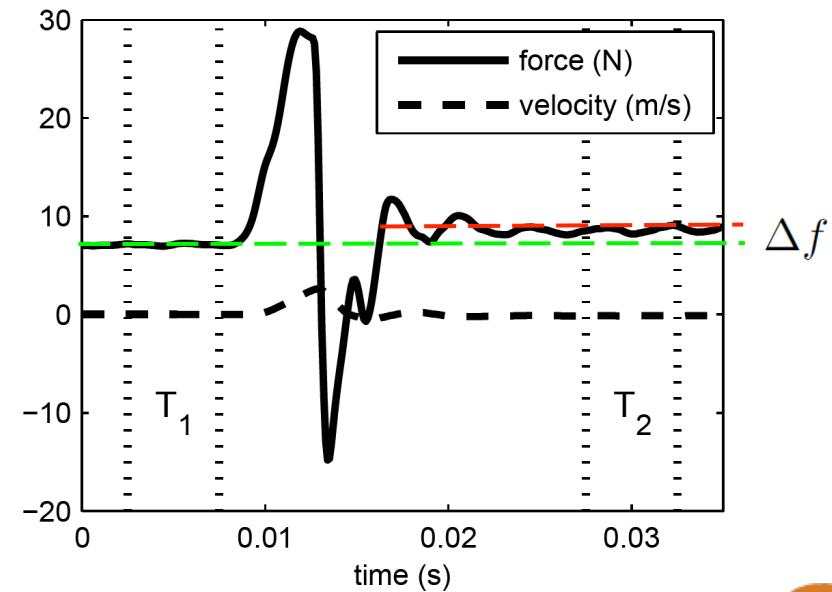
- Static measurement [Mussa-Ivaldi85]

$$m\ddot{x}(t) + r\dot{x}(t) + kx(t) = f(t) \longrightarrow k = \frac{E_{T_2}(f) - E_{T_1}(f)}{E_{T_2}(x) - E_{T_1}(x)}$$

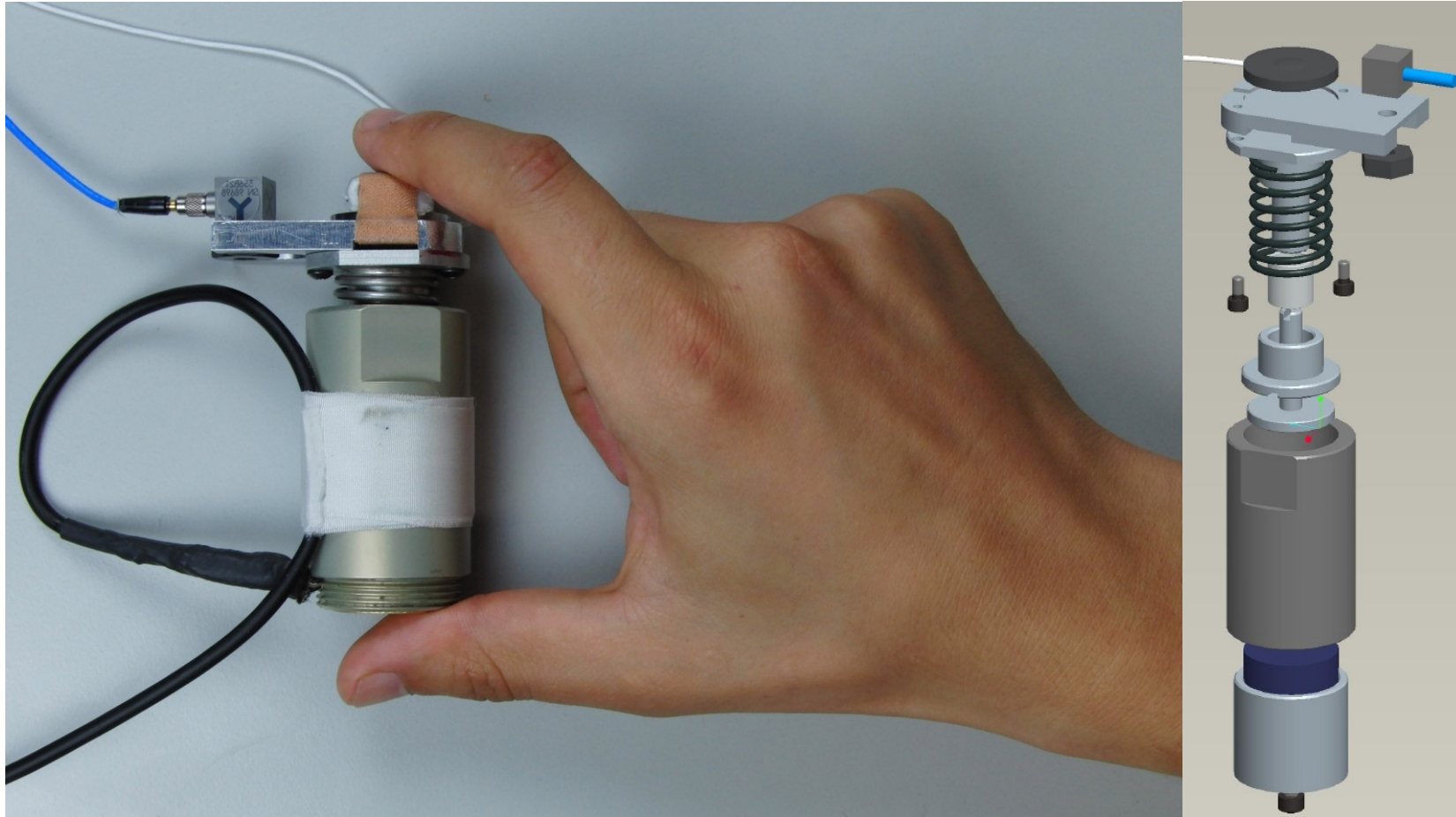
- Measurement time $t \approx 30 \text{ ms}$ and thus below human finger reflex time
- Constant initial position and displacement. $\Delta x = \text{const.}$ $x_0 = \text{const.}$



patent pending



measurement device

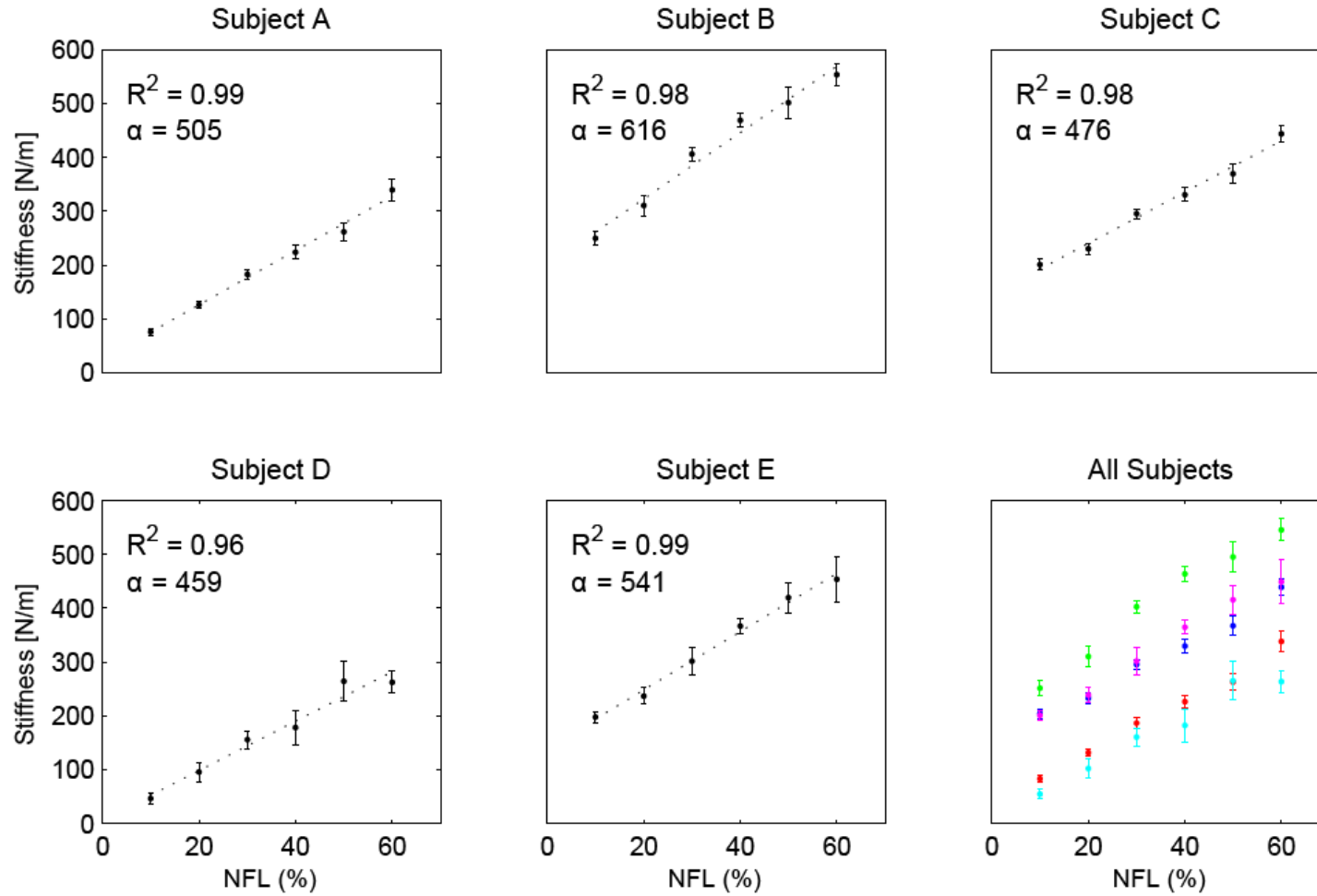


experiment and measurement procedure

- 5 healthy male subjects using Pinch Grasp
- Grasp Perturbator without any fixation
- 1. Subjects Maximum Gripping Force is estimated
- 2. Subject is asked to apply Normalized Force Levels ***NFL***
 - Reaching NFL using 2 Bands (85% and 115%)
- 3. $2 < T < 4$ seconds after the force is reached a Perturbation is applied



Results



conclusion

- **what does the linear relation imply?**

$$K = \frac{\partial F}{\partial x} = c_1 \cdot F(x) + c_2 \longrightarrow$$

*linear relation at the elbow between torque and stiffness
[Bennett93]*

tendons can be assumed as exponential elements [Glantz74]

- **How does this contribute to robotics?**
guideline for VSA



leftovers from this week

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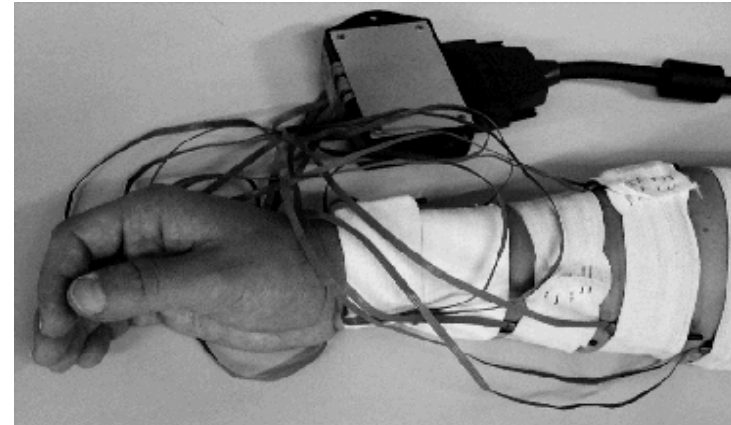
claudio castellini

□ Ph.D, U. Edinburgh

□ research topic:
hand prosthetics and
rehabilitation



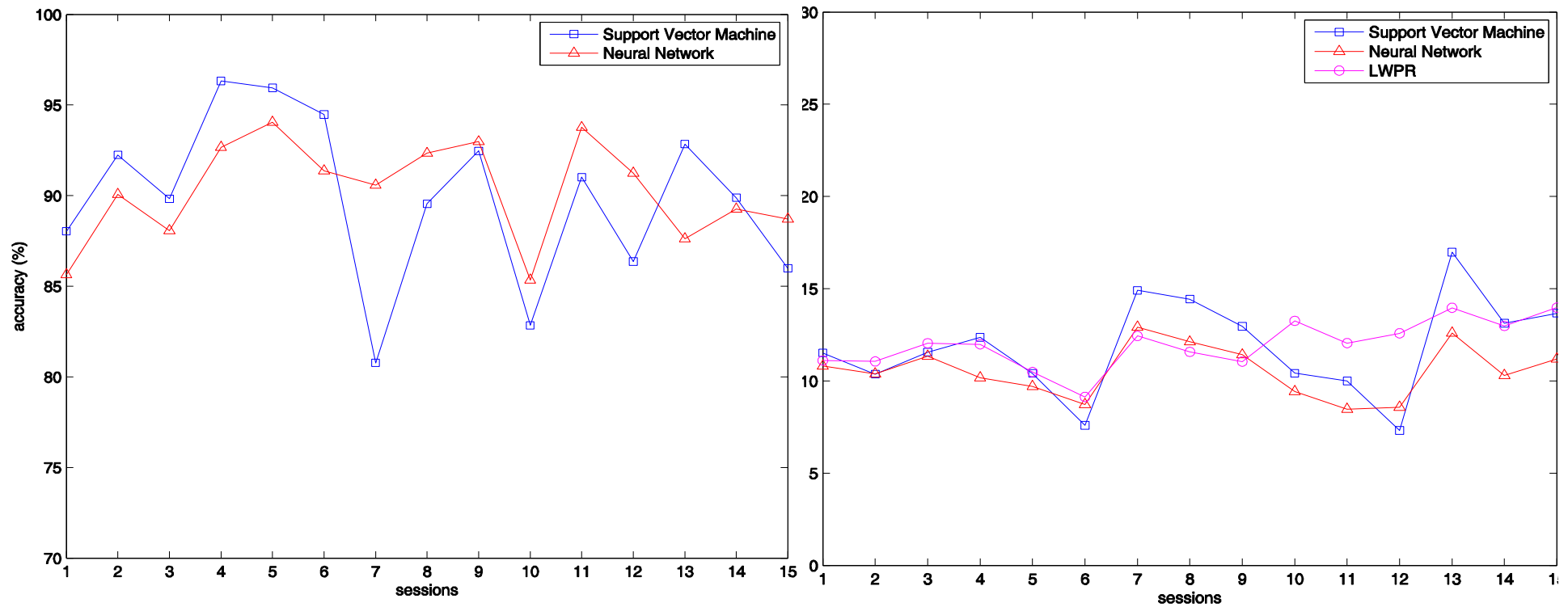
finger position and force from EMG



- 10 Ottobock emg electrodes
- 1 force/torque sensor
- 4 fingertip force sensors



high-precision EMG



best models on day 1, classification accuracy (left) and regression NRMSE (right)

accuracy ~ 10%



PNS-based robot control: EMG



jörn [yearn] vogel



high-precision EMG

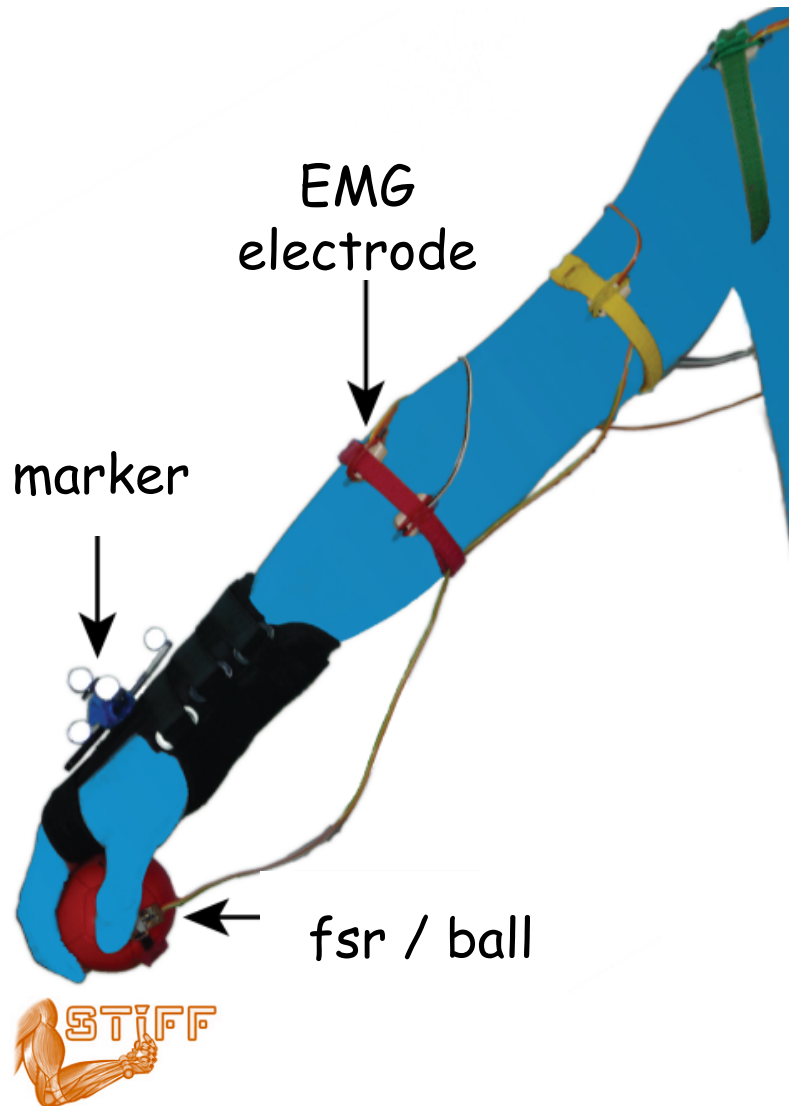
hand emg:

- static finger forces
- limited accuracy (~10%), but this is not evident
- qualitative visual feedback solves limited accuracy

arm emg:

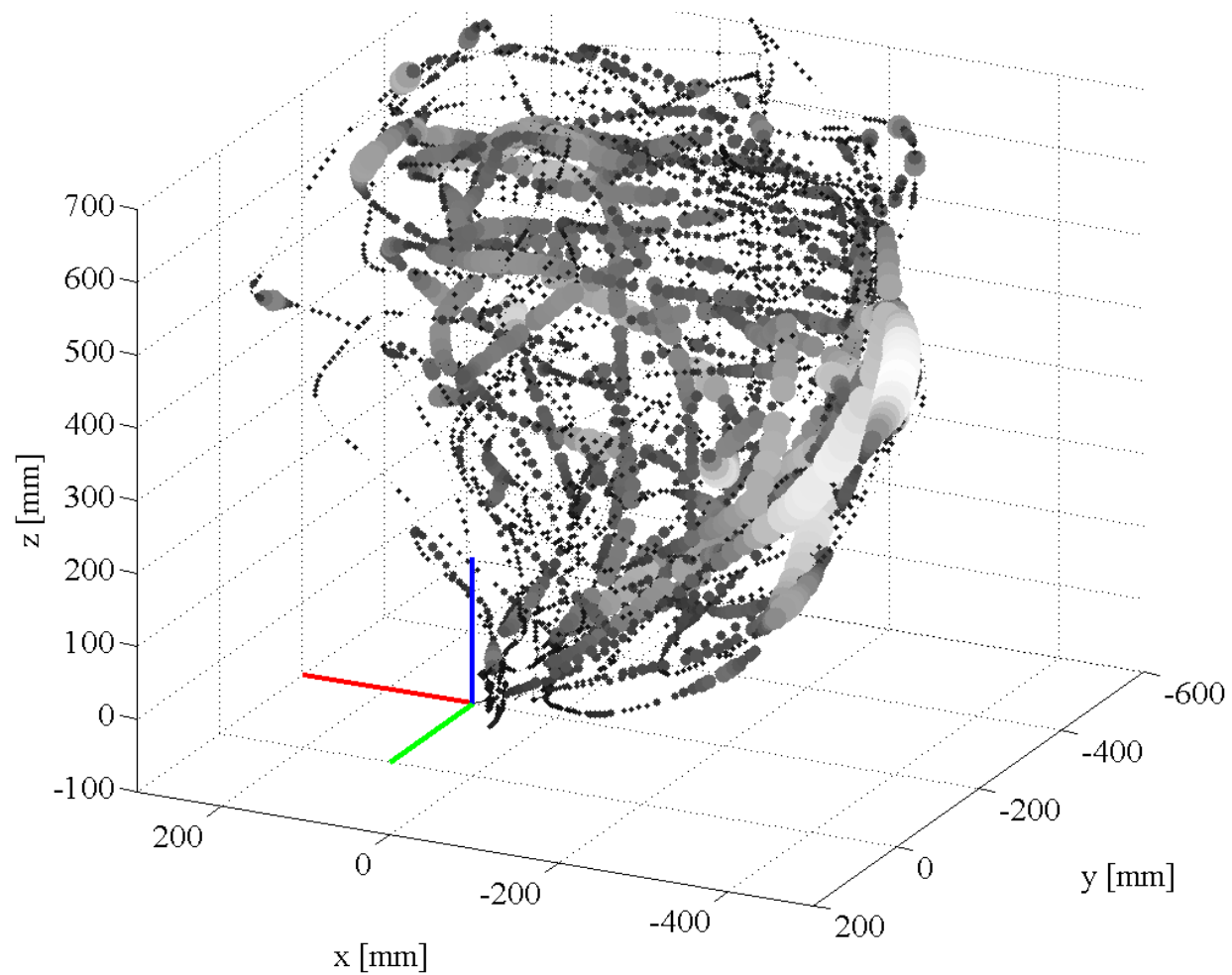


extension by adding 6-DoF arm dynamics



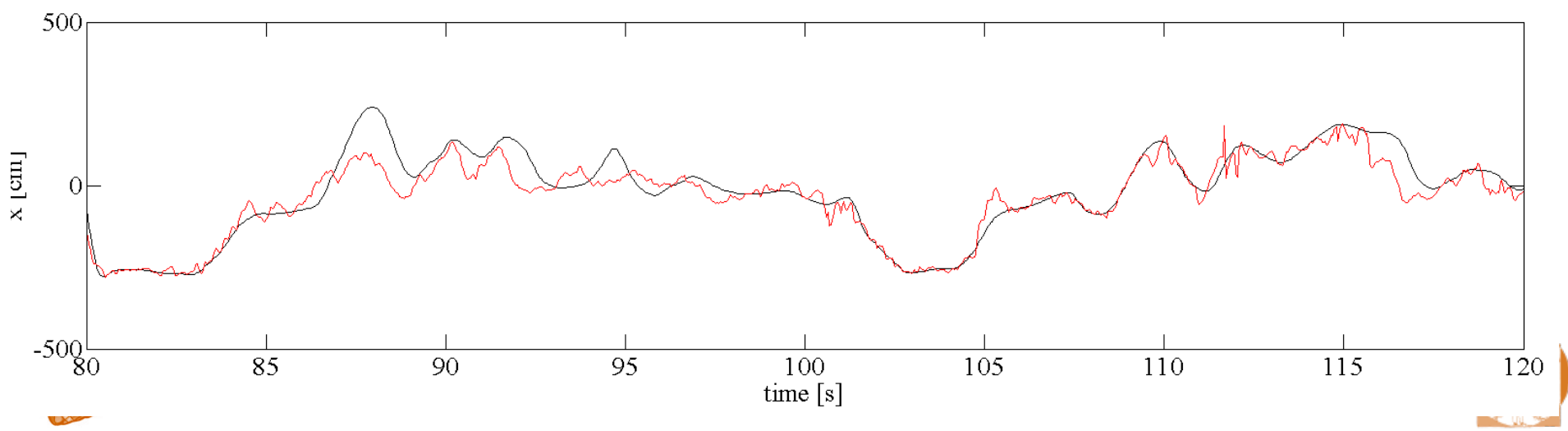
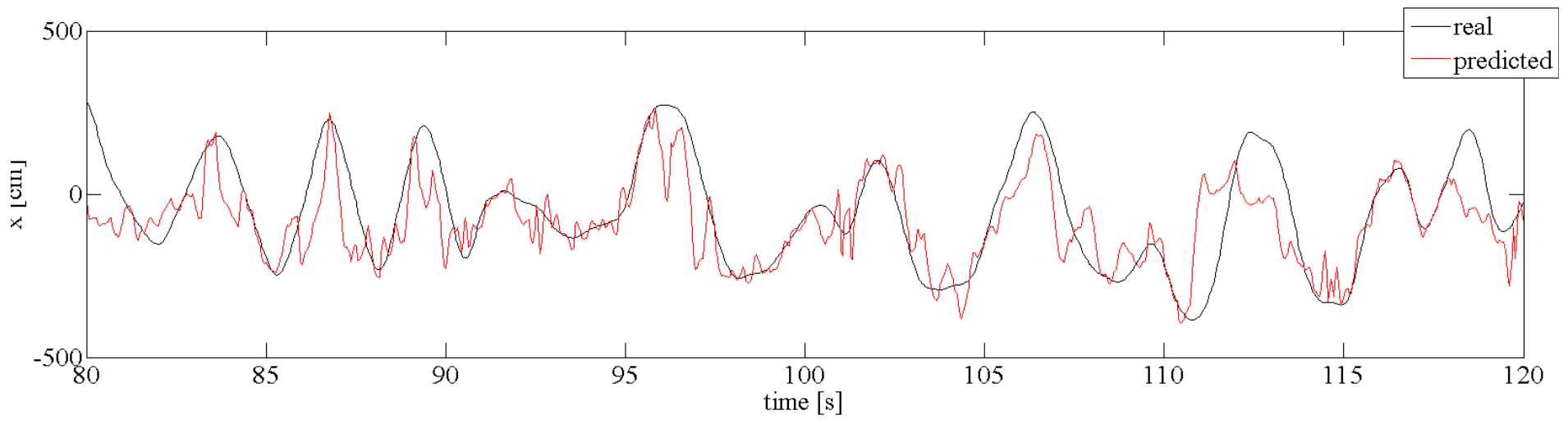
- emg signal no longer statically related to position or force
- emg activity related to gravity, commanded impedance, and acceleration
- we expect increased muscle activity close to target (Burdet *et al's*, Nature, 2001: increased stiffness in divergent fields)
- task-oriented training (TA)





larger and lighter indicates a larger error





high-precision EMG

hand emg:

- static finger forces
- limited accuracy (~10%), but this is not evident
- qualitative visual feedback solves limited accuracy

arm emg:

increase emg complexity to dynamic arm control

limited accuracy (~5%) is eminent (high accuracy is required)

qualitative feedback required!



how can we improve the accuracy of the system?

- remove "static" emg signal related to gravity by using blind source separation
- improve the accuracy by introducing *acceleration-based* control out of the remaining emg signal
- applicability to robotic rehabilitation

